

COATING TECH
SLOT DIES

PROCESS KNOWLEDGE • PRECISION • PERFORMANCE



THE EFFECTS OF VISCOELASTIC BEHAVIOR ON COATING

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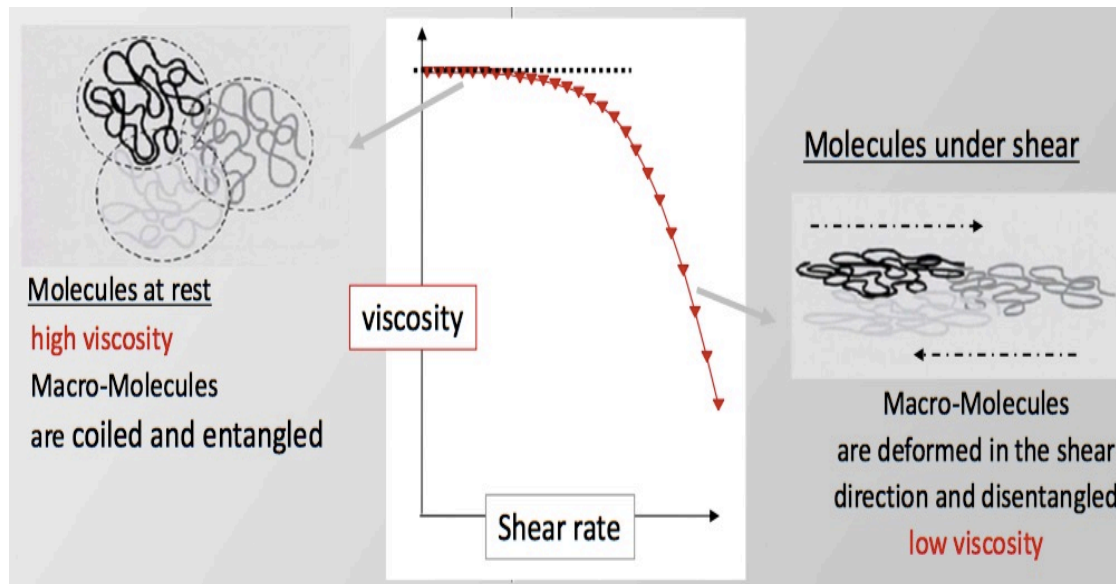
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VISCOELASTICITY

- Viscosity (shear rate versus viscosity)
- Elasticity (stress and velocity interaction)



The science of slot dies

VISCOSITY

- (complex) Rheology = a curve, not a point
- Storage and Loss Modulus (G' & G'') = spring constant (PE & KE)
- Molecular Weight (distribution)

Shear stress

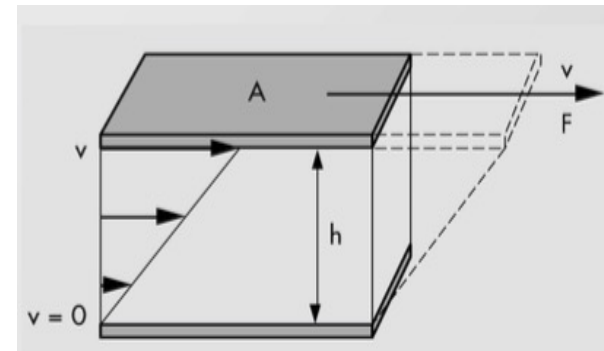
$$\tau = \frac{F}{A} = \frac{\text{shear (force)}}{(\text{shear}) \text{ area}} = \frac{\text{N}}{\text{m}^2} = \text{Pa}$$

Shear rate

$$\dot{\gamma} = \frac{v}{h} = \frac{\text{velocity}}{\text{gap}} = \frac{\text{m/s}}{\text{m}} = \frac{1}{\text{s}}$$

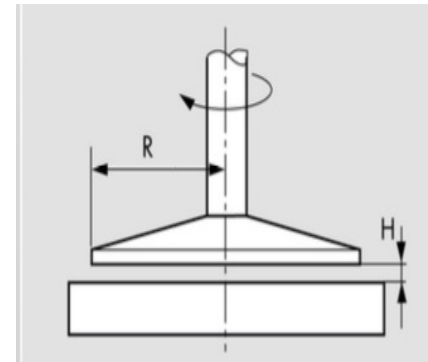
Viscosity

$$\eta = \tau \div \dot{\gamma}$$



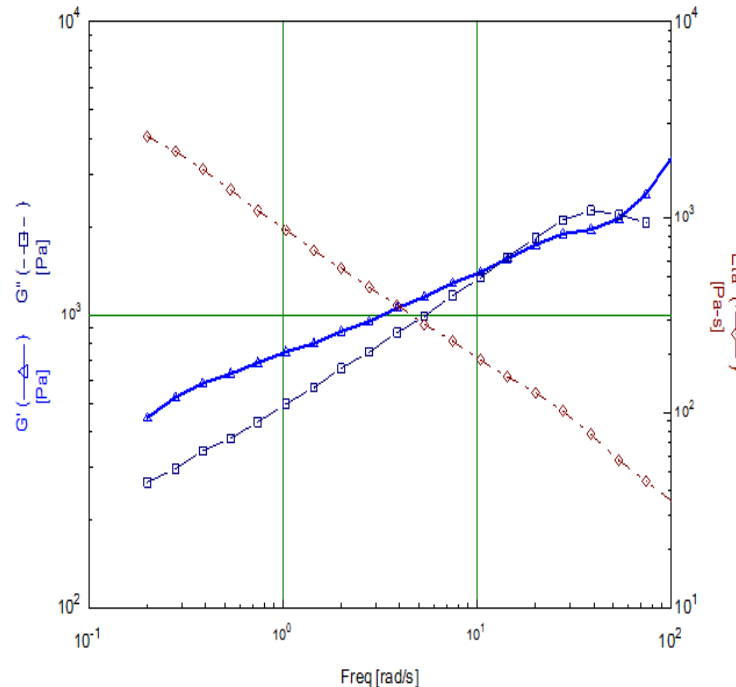
VISCOSITY

- (MORE complex) Rheology = hysteresis
- Stress-relaxation
 - Snap back (lack of self-leveling)
 - Expansions and Contractions (manifold design)
- Film split



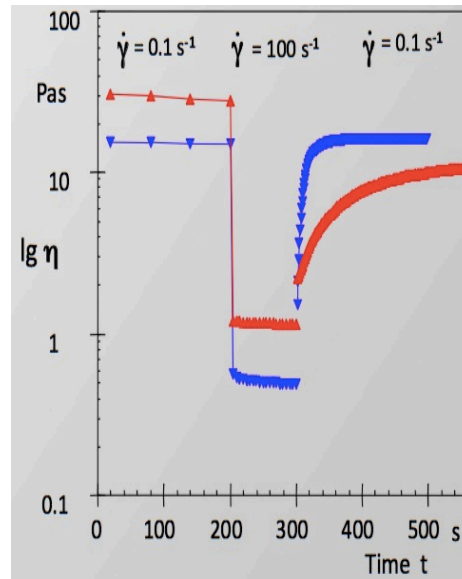
VISCOSITY

- $\tan \delta = G''/G'$ (balance of viscoelastic behavior)



ELASTICITY

- No modulus dependence on time
- Elongational testing (rough or elegant)



RHEOLOGY & COATING

- Reynolds $Re = \rho V L / \mu$ (inertial forces) / (net viscous force)
- Capillary $Ca = \mu V / \sigma$ (viscosity induced pressure gradient) / (capillary pressure)
- Stokes $St = \rho g L^2 / \mu V$ (gravity force) / (net viscous force)
- Elasticity $El = \mu V / EL$ (viscous stress) / (elastic stress in boundary)
- Deborah $De = \lambda V / L$ (elastic stress within liquid) / (viscous stress)

The science of slot dies

COATING

- Recognized phenomenon
- Defect analysis
- Crossroads of liquid coating and polymer extrusion



The science of slot dies

COATING

- Viscoelasticity dominates, then time dependent stress

$$E_r(t) = \frac{\sigma(t)}{\epsilon_0}$$

$E_r(t)$ = *stress relaxation modulus*

$\sigma(t)$ = *stress*

ϵ_0 = *applied strain*

- Time is greater at lower temperatures

COATING

- Film split
 - Misting
 - Roll spatter (high MW = more splatter)



$$\frac{\Delta P}{\Delta X} = 12\mu \left(\frac{\frac{(U_1 + U_2)}{2}}{H^2} - \frac{Q}{H^3} \right)$$

P = pressure

X = distance

μ = viscosity

U_1 & U_2 = roll speeds

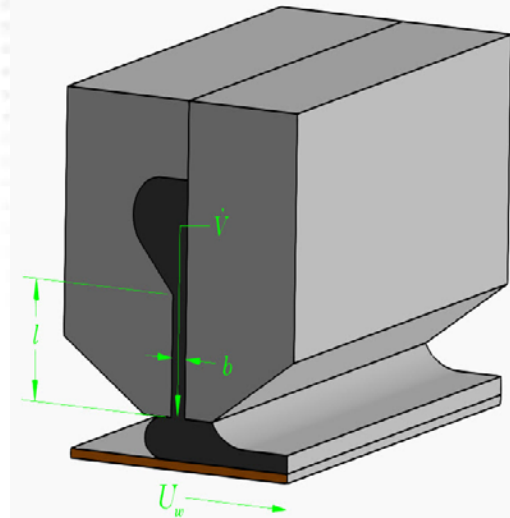
Q = volumetric flow rate

H = separation between roll surfaces

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COATING

- Pre-metered flow control
 - Forced flow (no self-leveling)
 - Die swell (edge bead)
 - Neck-in (speed effects)
 - Retraction (wrinkling, curl or voids)

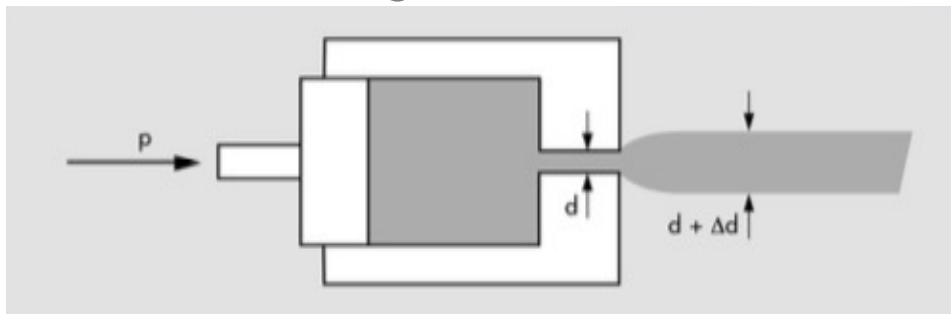


\dot{V} = FLOW RATE

μ = VISCOSITY

l = SLOT LENGTH

b = SLOT WIDTH



$$\dot{V} = \frac{\Delta p b^3}{12 \mu L}$$

The science of slot dies

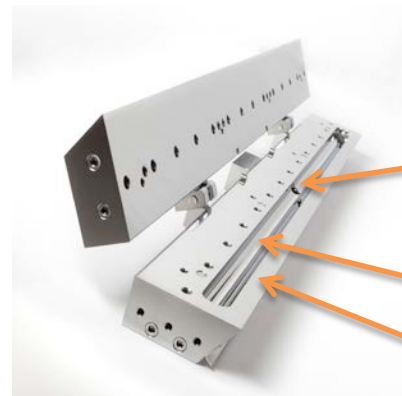
COATING

- Pre-metered flow control



Slot gap

$$\dot{V} = \frac{\Delta p b^3}{12 \mu L}$$



Feed
port

Distribution
chamber
Lip land

The science of slot dies

COATING

- 2D non-Newtonian flow models (internal flow)

- Casson (short time model) $\sqrt{\tau_{xy}} = \sqrt{\tau_0} + \sqrt{\eta} \sqrt{\gamma_{xy}}$

τ_{xy} = shear stress

τ_0 = apparent yield stress

η = viscosity

γ_{xy} = rate of strain

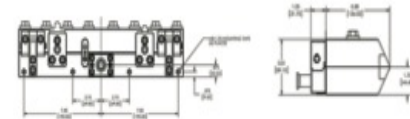
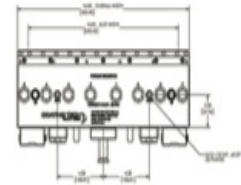
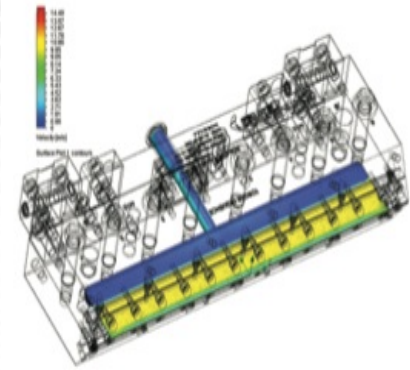
- Maxwell (long time model)

$$\tau_{xy} + \frac{\eta}{G} \frac{d\tau_{xy}}{dt} = -\eta \gamma_{xy}$$

G = elastic shear modulus

COATING

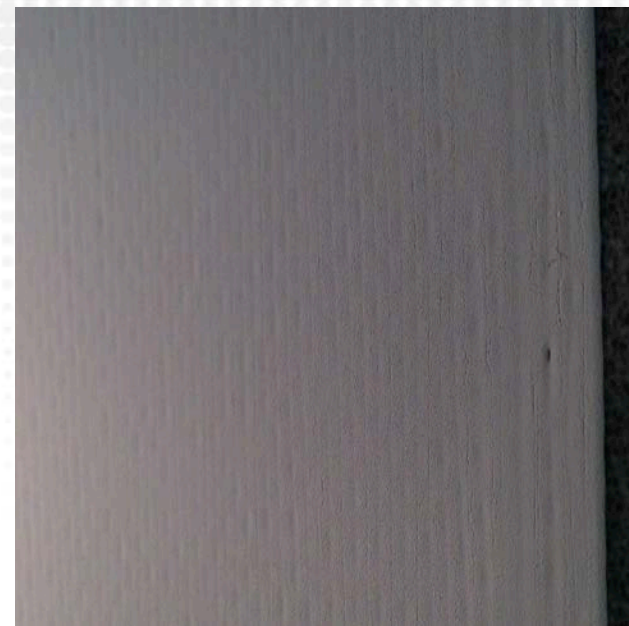
- 3D Finite Element Analysis (defined boundary conditions)
 - Stress Relaxation
 - Time-Temperature and Boltzmann Superposition principles
 - Creep (long time frames)



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COATING

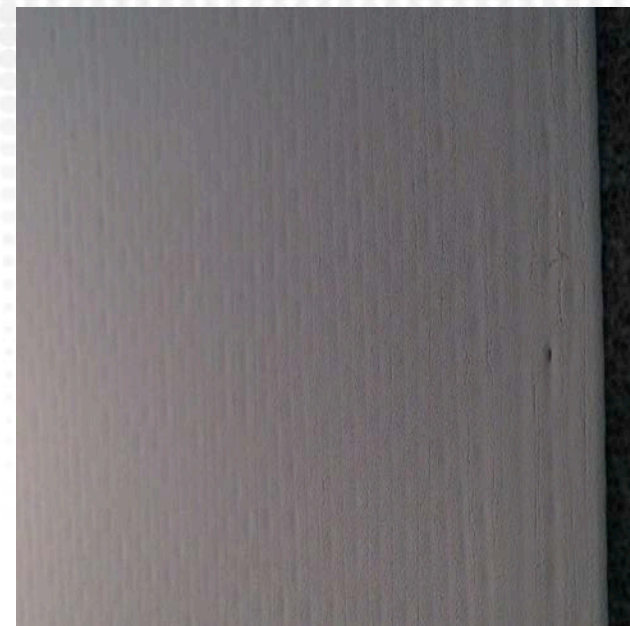
- Defects
 - Coating while stressed (ribbing, neck-in and edge bead/die swell)
 - Curing while stressed (wrinkle, curl and voids)



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COATING

- Solutions
 - Ribbing = positional adjustment
 - Edge bead = slot to substrate gap
 - Neck-in = speed related
 - Wrinkle/Curl = reduce stress at coating or during curing
 - Voids = limit of process



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SUMMARY



- Viscoelasticity is complex – test appropriately
- Reduce stress to improve coating
- Implement mathematical understanding to coating process development
- Coating window is fundamentally reduced because of viscoelastic behavior



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