

New Developments in Strain Hardening Modulus for Polyethylene Pressure Piping Applications

Dr. Bryan E. Hauger
Bryan Hauger Consulting, Inc.

POLYOLEFINS CONFERENCE
February 26 - March 1, 2017
Houston, Texas



Overview

- Objectives
- Introduction
 - Strain Hardening Modulus (SHM) and Natural Draw Ratio (NDR)
- Case Studies
 - 2005 – The Origin of ISO 18488
 - 2012 – Statistics of SHM
 - 2015 – Early Log PENT / SHM correlation
 - 2016 – Log PENT / ISO 18488 SHM correlation
- Statistical Analysis
- Current ASTM Work
- Conclusions



Objectives

- Introduce ISO 18488 test method for measurement of strain hardening modulus (SHM)
- Illustrate the promise of SHM to replace the PENT test
- Provide some statistical context to the ISO 18488 test
- Update the status of efforts to introduce an ASTM test method for SHM



Background on SCG

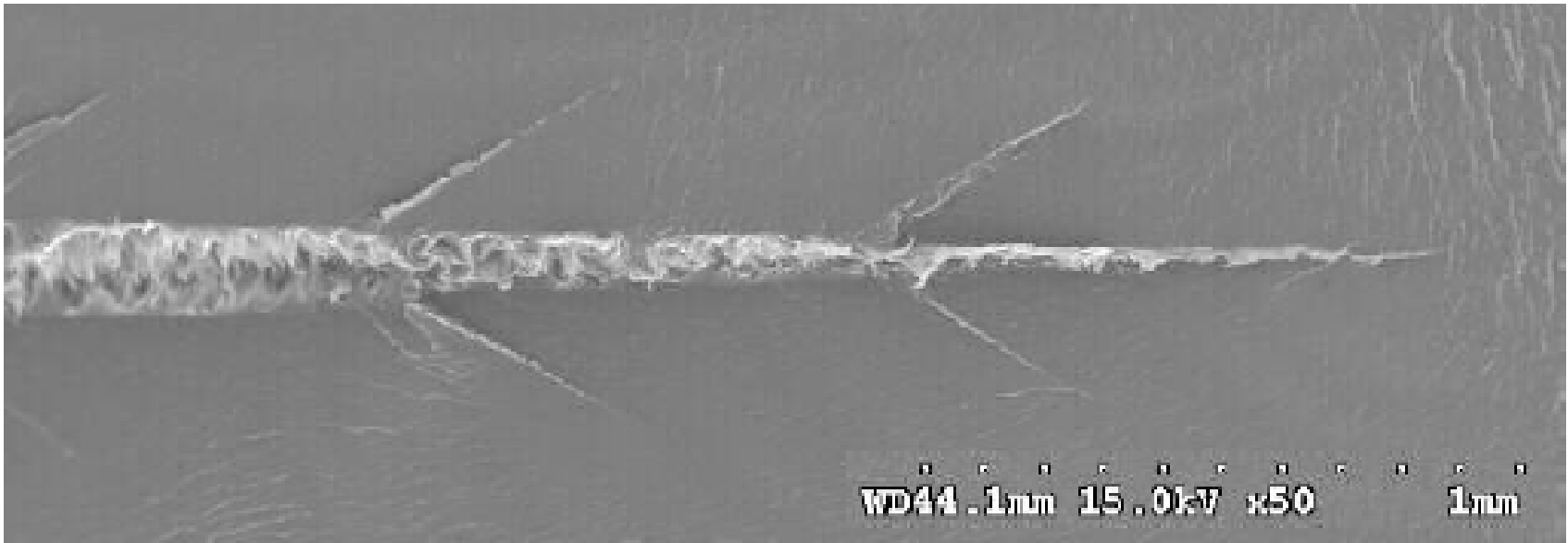
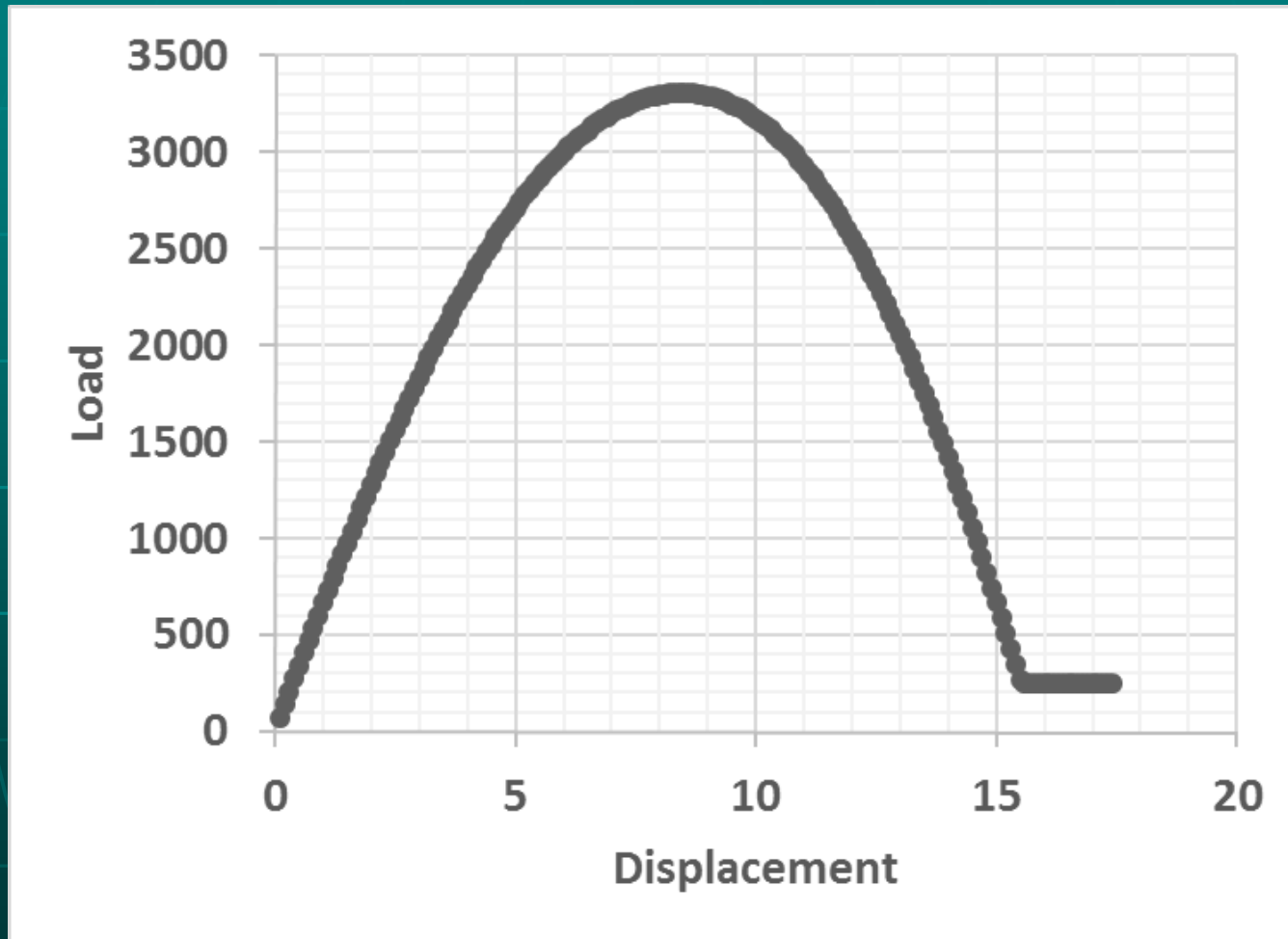


Image from Z. Zhou, et. al "Temperature Effects on Slow Crack Growth in Pipe Grade PE", SPE ANTEC Proceedings, 2010, p. 680.

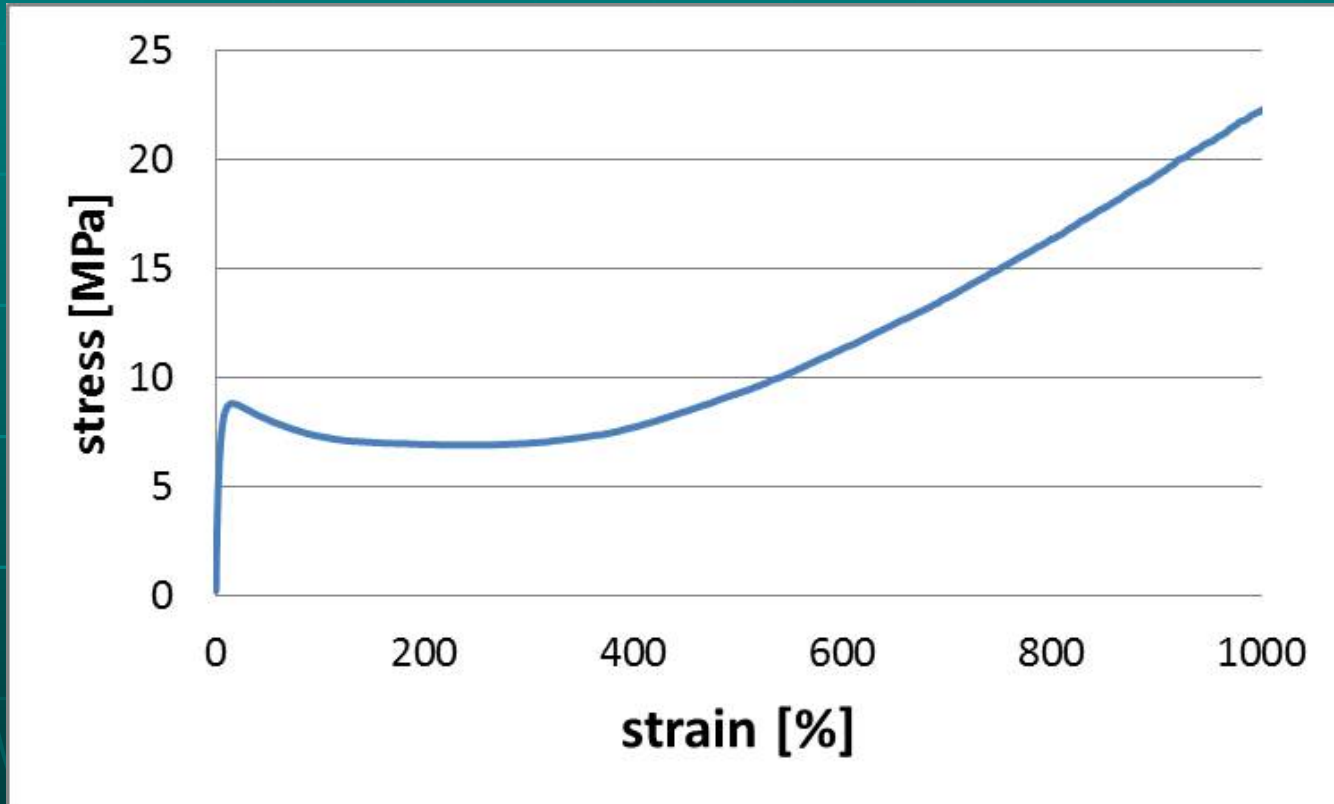
Bryan Hauger Consulting, Inc. – February 2017



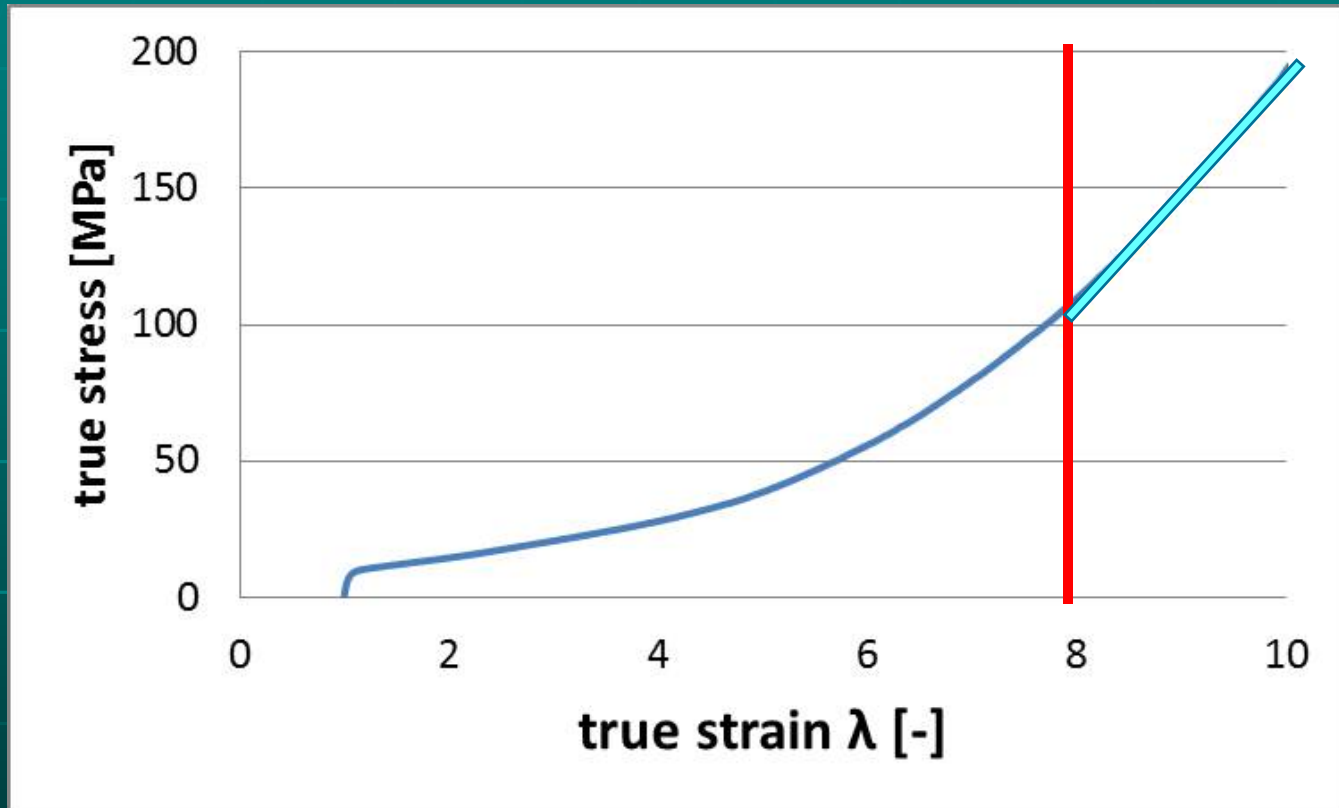
Stress Strain Curve for PE



Stress Strain Curve for PE



True Stress Strain Curve for PE



2005 – The Origin of SHM

- "Strain Hardening Modulus As a Measure of Environmental Stress Crack Resistance of High Density Polyethylene" Polymer, 46, (2005), 6369-6379.
- Blow molding and pipe resins were subjected to both "standard tensile ESCR test" at 75C and an ISO37 type 3 tensile bar at 80C and elongation at 10 mm/min using an optical extensometer

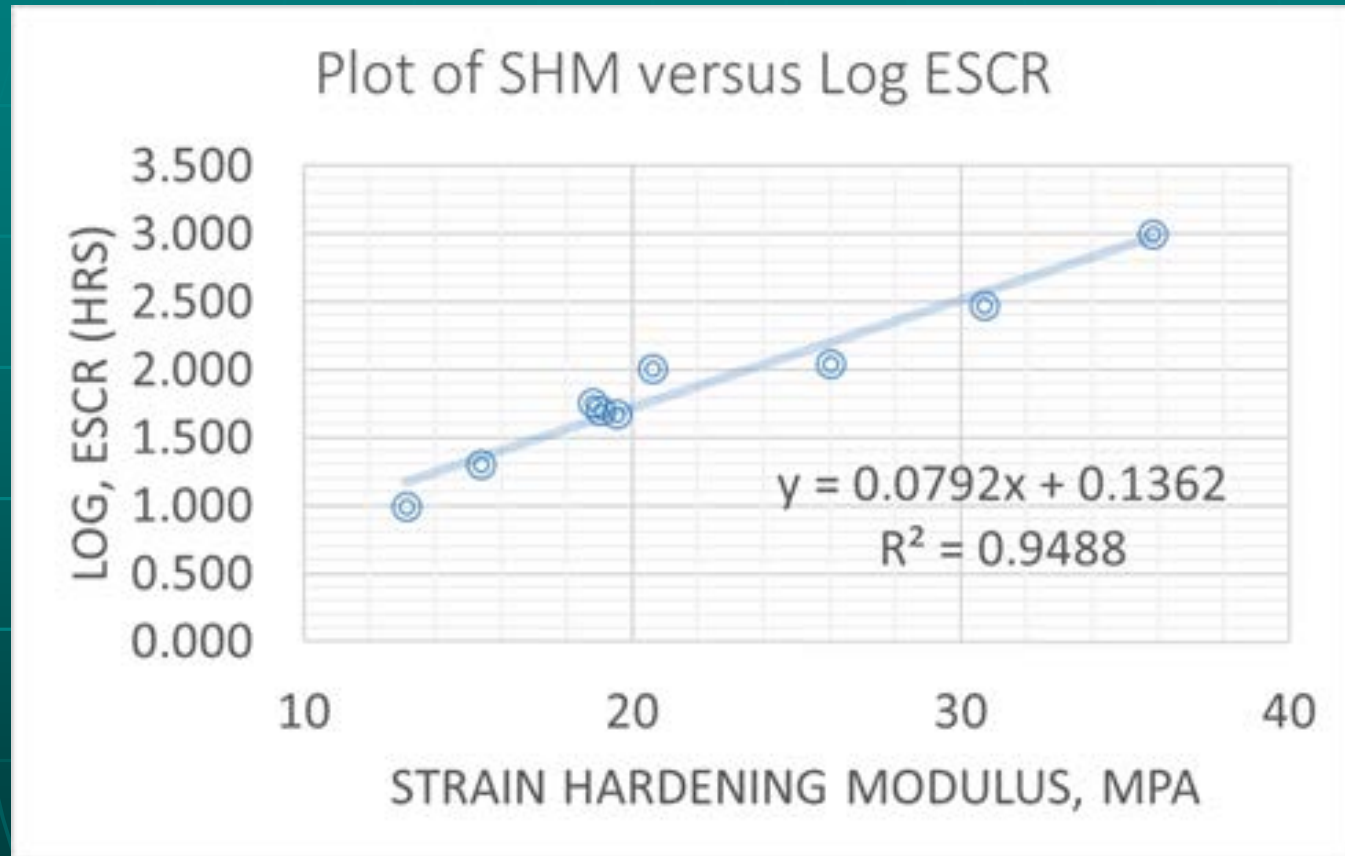


2005 – The Origin of SHM

| ESCR (hrs) | SHM | Log ESCR |
|---------------|------|-------------|
| 10 | 13.1 | 1.000 |
| 20 | 15.4 | 1.301 |
| 47 | 19.5 | 1.672 |
| 50 | 19 | 1.699 |
| 58 | 18.8 | 1.763 |
| 103 | 20.6 | 2.013 |
| 112 | 26 | 2.049 |
| 300 | 30.7 | 2.477 |
| 1000 | 35.8 | 3.000 |
| >2000 | 47.2 | NA |



2005 Case Study - SHM versus Log ESCR



2005 Case Study – Molding and Testing

- Press into a sheet at 160°C with a thickness of about 0.3 mm by;
 - heating for 5 minutes at 0 kN load then 3 min at 10 kN load followed by 3 min at 50 kN load and finally cooling to RT at a load of 180 kN
- Anneal for 1 h at 120°C and then slow cool to RT by switching off the heat to the chamber.
- Test specimens (ISO37 type 3) are punched from the pressed sheets.
- 80°C tensile testing with a strain rate of 10 mm / minute and measured by optical extensometer



ISO 18488 Molding

- Press into a sheet at 180°C of thickness either 0.30 (+0.03 / -0.05) mm or 1.00 (± 0.1 mm) by;
 - heating for 5 to 15 minutes at 0 kN load then 5 +/- 1 min at 5 Mpa load followed by cooling to RT under load at 15 +/- 2°C
- Anneal for 1 h at 120 +/- 2 °C and then slow cool to < 40°C with an ave. cooling rate < 2 °C / min.
- Test specimens are slightly modified in Geometry from ISO37 type 3 bars
- 80°C tensile testing with a strain rate of 20 mm / minute and measured by optical extensometer



2012 - Statistics of SHM

| | Resin A | Resin B | Resin C |
|-----------------------------|---------|---------|---------|
| G_p in MPa | 82.7 | 46.6 | 25.1 |
| Standard Deviation | 8.0 | 2.3 | 1.1 |
| % Standard Deviation | 9.7 | 4.9 | 4.4 |



2015 – Log PENT and SHM

- “The Effect of Microstructure on the Slow Crack Growth Resistance in Polyethylene Resins” J. Polym. Eng. Sci., 55, 1018 – 1023 (2015).
- The paper reports work on “polyethylene grades from blow molding up to PE-80, PE-100, and higher resistant to crack grades”.

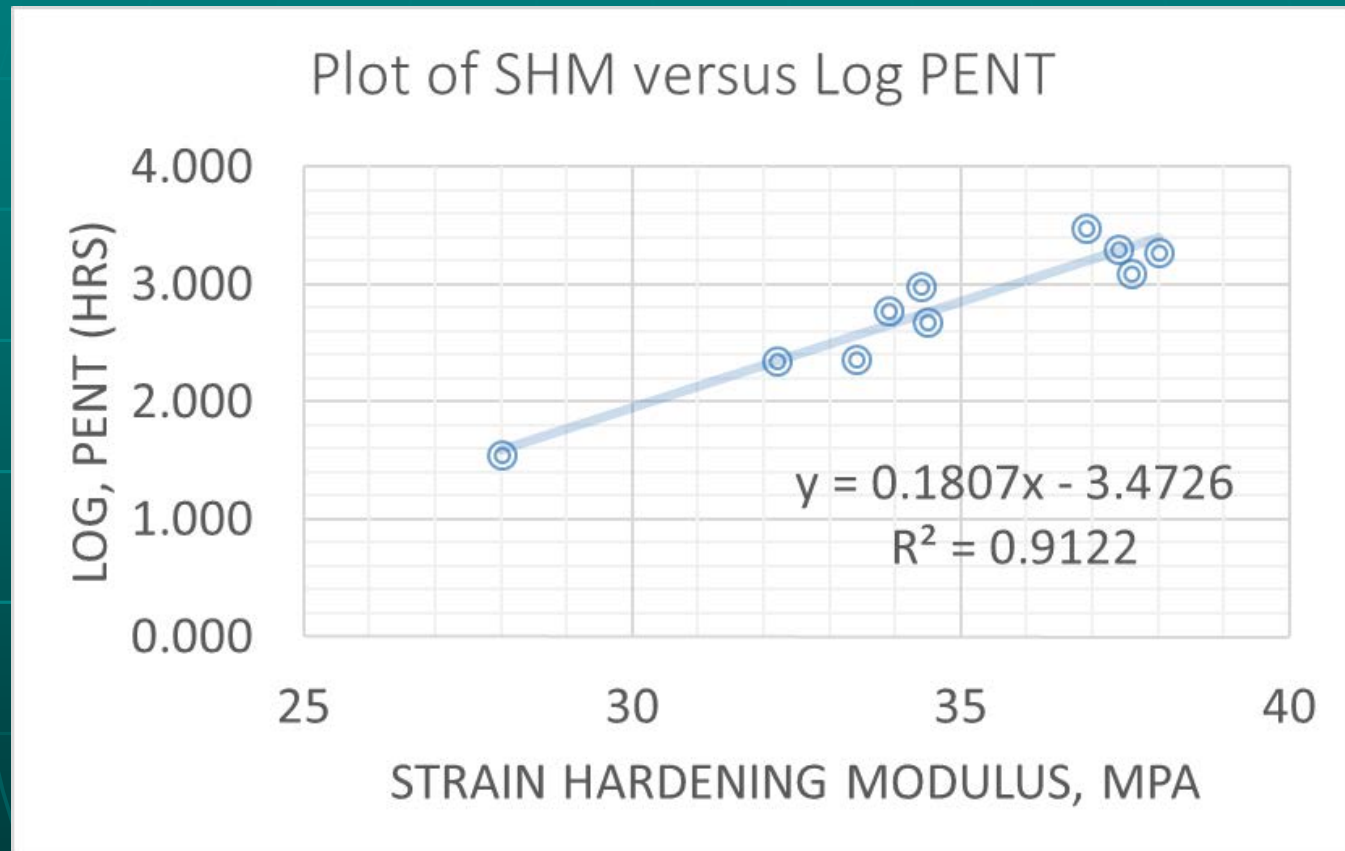


2015 – Correlation of Log PENT with SHM

| PENT (est.) (hrs) | Est. G_p MPa | Log PENT |
|----------------------|-------------------|----------|
| 35 | 28.0 | 1.544 |
| 225 | 32.2 | 2.352 |
| 230 | 33.4 | 2.362 |
| 475 | 34.5 | 2.677 |
| 600 | 33.9 | 2.778 |
| 950 | 34.4 | 2.978 |
| 1250 | 37.6 | 3.097 |
| 1875 | 38.0 | 3.273 |
| 2000 | 37.4 | 3.301 |
| 3025 | 36.9 | 3.481 |



2015 Correlation of SHM with Log PENT

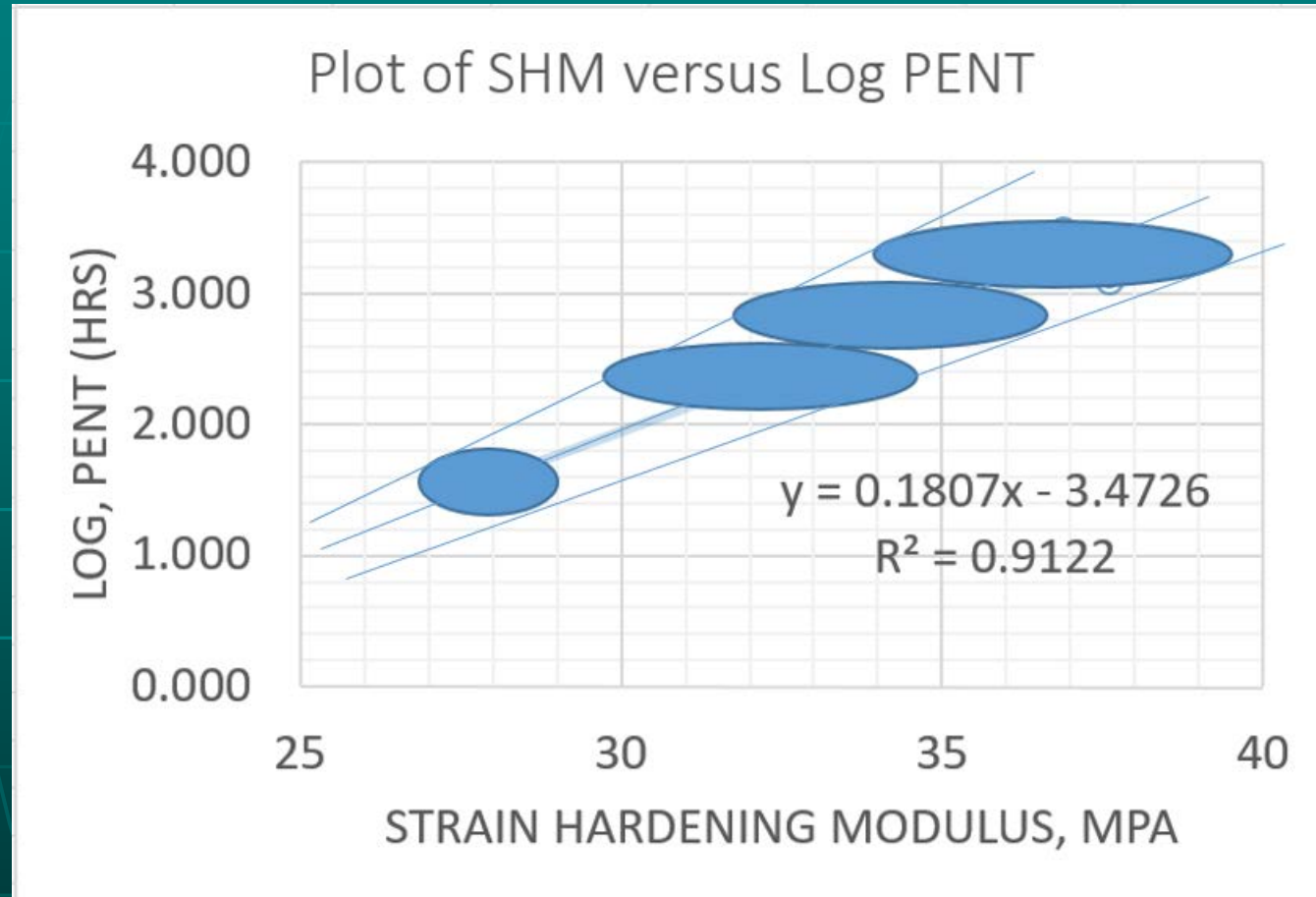


Statistical Synthesis on 2015 Data

| PENT (est.) (hrs) | Est. G_p MPa | 3 X Est. Standard Deviation, Mpa | Log PENT |
|-------------------------|-------------------|---|----------|
| 35 | 28.0 | 4.2 | 1.544 |
| 225 | 32.2 | 4.8 | 2.352 |
| 230 | 33.4 | 5.0 | 2.362 |
| 475 | 34.5 | 5.2 | 2.677 |
| 600 | 33.9 | 5.1 | 2.778 |
| 950 | 34.4 | 5.2 | 2.978 |
| 1250 | 37.6 | 5.6 | 3.097 |
| 1875 | 38.0 | 5.7 | 3.273 |
| 2000 | 37.4 | 5.6 | 3.301 |
| 3025 | 36.9 | 5.5 | 3.481 |



Statistical Synthesis on 2015 Data



2016 Correlation of SHM with Log PENT

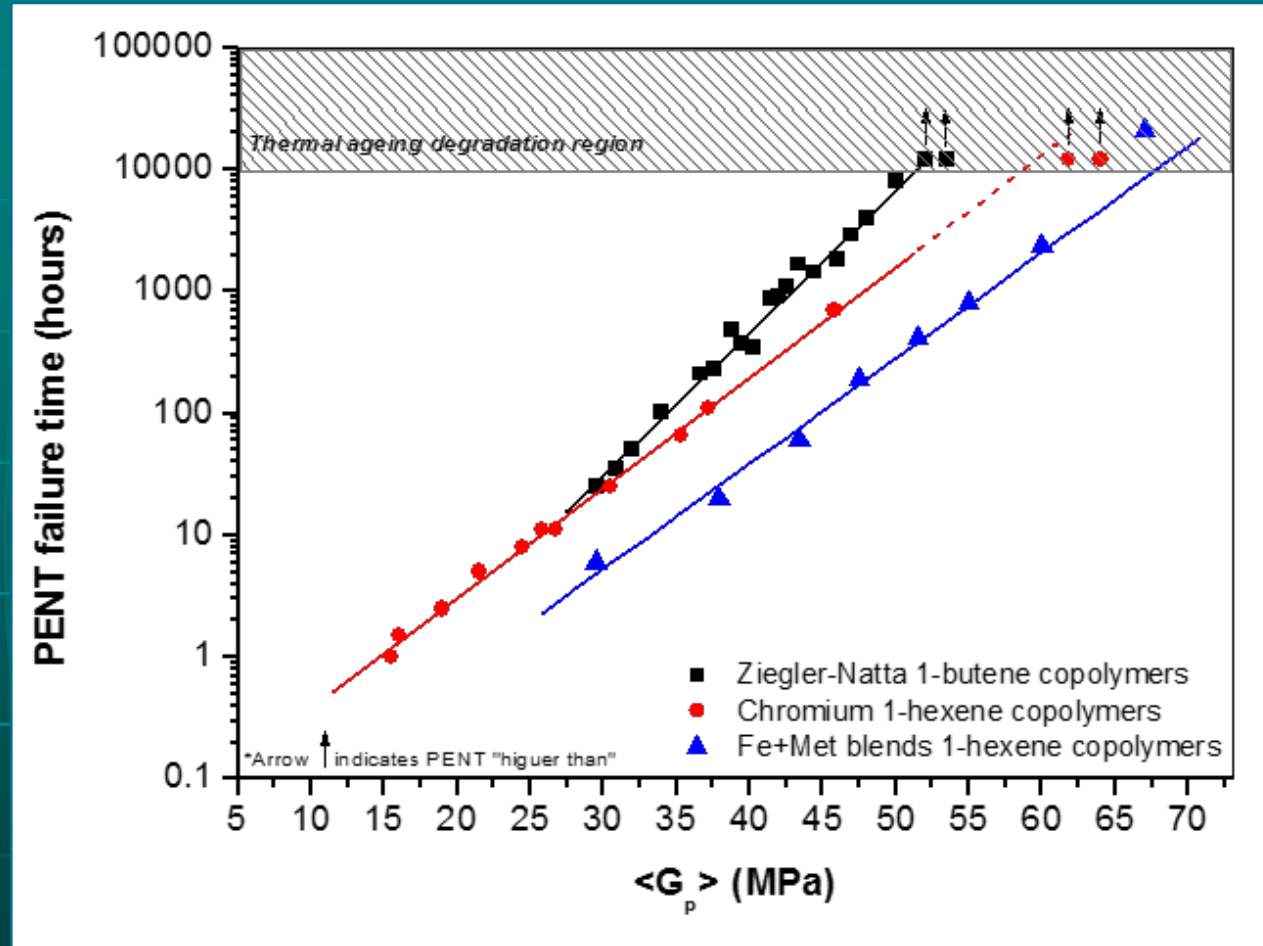


Image from C. Domínguez, et. al "Limits on the Slow Crack Growth Resistance Evaluation for the PE100 and PE100RC Polyethylene Resins". Plastics Pipes XVIII, Munich, Germany, September 2016.

Current ASTM Work

- ASTM test method titled “Measurement of Strain Hardening Modulus on Polyethylene Materials used in the Manufacture of Stress-Rated Pipe”.
- Once that Test Method is agreed upon in the consensus process, then work will start to include precision and bias testing
- Document if pigments including carbon black are tolerated



Conclusions

- ISO 18488 is the basis of current industry efforts to measure SHM.
- The ability to use SHM to obtain a correlation to PENT on PE pressure pipe resins is documented and supported by statistical analysis.
- An ASTM test method is currently under development which should address any remaining barriers to industry adoption.



Questions

